

Sample Calculations

Sample Calculations, Stack Outlet, Method 5B/202, Run 1

Area of Sample Location

$$A_s = \pi \times \left(\frac{d_n}{2 \times 12} \right)^2$$

$$A_s = \pi \times \left(\frac{180}{2 \times 12} \right)^2$$

$$A_s = 177 \text{ ft}^2$$

where:

- A_s = area of sample location (ft²)
- d_s = diameter of sample location (in)
- 12 = conversion factor (in/ft)
- 2 = conversion factor (diameter to radius)

Stack Pressure Absolute

$$P_a = P_b + \frac{P_s}{13.6}$$

$$P_a = 29.45 + \frac{-0.2}{13.6}$$

$$P_a = 29.44 \text{ in. Hg}$$

where:

- P_a = stack pressure absolute (in. Hg)
- P_b = barometric pressure (in. Hg)
- P_s = static pressure (in. H₂O)
- 13.6 = conversion factor (in. H₂O/in. Hg)

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Volume of Dry Gas Collected Corrected to Standard Temperature and Pressure

$$V_{m(std)} = \frac{17.64(V_m)(Y_d)\left(P_b + \frac{\Delta H}{13.6}\right)}{(T_m + 460)}$$

$$V_{m(std)} = \frac{17.64(63.56)(1.0034)\left(29.45 + \frac{1.64}{13.6}\right)}{(92.0 + 460)}$$

$$V_{m(std)} = 60.27 \text{ scf}$$

where:

| | |
|--------------|--|
| $V_{m(std)}$ | = volume of gas collected at standard temperature and pressure (scf) |
| V_m | = volume of gas sampled at meter conditions (ft ³) |
| Y_d | = gas meter correction factor (dimensionless) |
| P_b | = barometric pressure (in. Hg) |
| ΔH | = average sample pressure (in. H ₂ O) |
| T_m | = average gas meter temperature (°F) |
| 13.6 | = conversion factor (in. H ₂ O/in. Hg) |
| 17.64 | = ratio of standard temperature over standard pressure (°R/in.Hg) |
| 460 | = conversion (°F to °R) |

Volume of Water Vapor Collected Corrected to Standard Temperature and Pressure

$$V_{w(std)} = 0.04715 \times (V_{wc} + V_{wsg})$$

$$V_{w(std)} = 0.04715 \times (186.4 + 18.4)$$

$$V_{w(std)} = 9.66 \text{ scf}$$

where:

| | |
|--------------|--|
| $V_{w(std)}$ | = volume of water vapor at standard conditions (scf) |
| V_{wc} | = weight of liquid collected (g) |
| V_{wsg} | = weight gain of silica gel (g) |
| 0.04715 | = volume occupied by one gram of water at standard temperature and pressure (ft ³ /g) |

Percent Moisture²

$$B_{ws} = 100 \times \left[\frac{V_{w(std)}}{(V_{m(std)} + V_{w(std)})} \right]$$

$$B_{ws} = 100 \times \left[\frac{9.66}{(60.27 + 9.66)} \right]$$

$$B_{ws} = 13.8\%$$

where:

- B_{ws} = moisture content of the gas stream (%)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- $V_{w(std)}$ = volume of water vapor at standard conditions (scf)
- 100 = conversion factor

Molecular Weight of Dry Gas Stream³

$$M_d = \left(44 \times \frac{\%CO_2}{100} \right) + \left(32 \times \frac{\%O_2}{100} \right) + \left(28 \times \frac{(\%N_2)}{100} \right)$$

$$M_d = \left(44 \times \frac{11.1}{100} \right) + \left(32 \times \frac{8.17}{100} \right) + \left(28 \times \frac{(81.0)}{100} \right)$$

$$M_d = 30.10 \text{ lb / lbmole}$$

where:

- M_d = molecular weight of the dry gas stream (lb/lb-mole)
- $\%CO_2$ = carbon dioxide content of the dry gas stream (%)
- 44 = molecular weight of carbon dioxide (lb/lb-mole)
- $\%O_2$ = oxygen content of the dry gas stream (%)
- 32 = molecular weight of oxygen (lb/lb-mole)
- $\%N_2$ = nitrogen content of the dry gas stream (%)
- 28 = molecular weight of nitrogen and carbon monoxide (lb/lb-mole)
- 100 = conversion factor

² The moisture saturation point is used for all calculations if it is exceeded by the actual moisture content.

³ The remainder of the gas stream after subtracting carbon dioxide and oxygen is assumed to be nitrogen.

Molecular Weight of Wet Gas Stream

$$M_s = \left(M_d \times \left(1 - \frac{B_{ws}}{100} \right) \right) + \left(18 \times \frac{B_{ws}}{100} \right)$$

$$M_s = \left(30.10 \times \left(1 - \frac{13.8}{100} \right) \right) + \left(18 \times \frac{13.8}{100} \right)$$

$$M_s = 28.43 \text{ lb / lbmole}$$

where:

- M_s = molecular weight of the wet gas stream (lb/lb-mole)
- M_d = molecular weight of the dry gas stream (lb/lb-mole)
- B_{ws} = moisture content of the gas stream (%)
- 18 = molecular weight of water (lb/lb-mole)
- 100 = conversion factor

Velocity of Gas Stream

$$V_s = 85.49 (C_p) \left(\sqrt{\Delta P} \right) \sqrt{\frac{(T_s + 460)}{(M_s) \left(P_b + \frac{P_s}{13.6} \right)}}$$

$$V_s = 85.49 (0.84) (1.45) \sqrt{\frac{(130 + 460)}{(28.41) \left(29.45 + \frac{-0.2}{13.6} \right)}}$$

$$V_s = 87.1 \text{ ft / sec}$$

where:

- V_s = average velocity of the gas stream (ft/sec)
- C_p = pitot tube coefficient dimensionless
- $\sqrt{\Delta P}$ = average square root of velocity pressures (in. H₂O)^{1/2}
- T_s = average stack temperature (°F)
- M_s = molecular weight of the wet gas stream (lb/lb-mole)
- P_b = barometric pressure (in. Hg)
- P_s = static pressure of gas stream (in. H₂O)
- 85.49 = pitot tube constant (ft/sec)/[(lb/lb-mole)(in. Hg)]/[(^{°R})(in. H₂O)]^{1/2}
- 460 = conversion (°F to °R)
- 13.6 = conversion factor (in. H₂O/in. Hg)

Volumetric Flow of Gas Stream - Actual Conditions

$$Q_a = 60(V_s)(A_s)$$

$$Q_a = 60(87.1)(177)$$

$$Q_a = 923,684 \text{ acfm}$$

where:

Q_a = volumetric flow rate of the gas stream at actual conditions (acfm)

V_s = average velocity of the gas stream (ft/sec)

A_s = area of duct or stack (ft²)

60 = conversion factor (min/hr)

Volumetric Flow of Gas Stream - Standard Conditions

$$Q_{std} = \frac{17.64(Q_a) \left(P_b + \frac{P_s}{13.6} \right)}{(T_s + 460)}$$

$$Q_{std} = \frac{17.64(923,684) \left(29.45 + \frac{-0.2}{13.6} \right)}{(130 + 460)}$$

$$Q_{std} = 813,132 \text{ scfm}$$

where:

Q_{std} = volumetric flow rate of the gas stream at standard conditions (scfm)

Q_a = volumetric flow rate of the gas stream at actual conditions (acfm)

T_s = average stack temperature (°F)

P_b = barometric pressure (in. Hg)

P_s = static pressure of gas stream (in. H₂O)

13.6 = conversion factor (in. H₂O/in. Hg)

17.64 = ratio of standard temperature over standard pressure (°R/in. Hg)

460 = conversion (°F to °R)

Volumetric Flow of Gas Stream - Standard Conditions - Dry Basis

$$Q_{dstd} = Q_{std} \left(1 - \frac{B_{ws}}{100} \right)$$

$$Q_{dstd} = 813,132 \left(1 - \frac{13.8}{100} \right)$$

$$Q_{dstd} = 701,128 \text{ dscfm}$$

where:

- Q_{dstd} = volumetric flow rate of the gas stream at standard conditions, on a dry basis (dscfm)
- Q_{std} = volumetric flow rate of the gas stream at standard conditions (scfm)
- B_{ws} = moisture content of the gas stream (%)
- 100 = conversion factor

Area of Nozzle

$$A_n = \pi \times \left(\frac{d_n}{2 \times 12} \right)^2$$

$$A_n = \pi \times \left(\frac{0.175}{2 \times 12} \right)^2$$

$$A_n = 0.000167 \text{ ft}^2$$

where:

- A_n = area of nozzle (ft²)
- d_n = diameter of nozzle (in)
- 12 = conversion factor (in/ft)
- 2 = conversion factor (diameter to radius)

Percent Isokinetic

$$I = \frac{0.0945(T_s + 460)(V_{m(std)})}{\left(P_b + \frac{P_s}{13.6}\right)(v_s)(A_n)(\Theta)\left(1 - \frac{B_{ws}}{100}\right)}$$

$$I = \frac{0.0945(130 + 460)(60.27)}{\left(29.45 + \frac{-0.2}{13.6}\right)(87.1)(1.67 \times 10^{-4})(90)\left(1 - \frac{13.8}{100}\right)}$$

$$I = 101.1\%$$

where:

| | |
|---------------------|--|
| I | = percent isokinetic (%) |
| T _s | = average stack temperature (°F) |
| V _{m(std)} | = volume of gas collected at standard temperature and pressure (scf) |
| P _b | = barometric pressure (in. Hg) |
| P _s | = static pressure of gas stream (in. H ₂ O) |
| V _s | = average velocity of the gas stream (ft/sec) |
| A _n | = cross sectional area of nozzle (ft ²) |
| Θ | = sample time (min) |
| B _{ws} | = moisture content of the gas stream (%) |
| 0.0945 | = constant (°R/in. Hg) |
| 460 | = conversion (°F to °R) |
| 13.6 | = conversion factor (in. H ₂ O/in Hg) |
| 100 | = conversion factor |

Acetone Wash Blank-Particulate

$$W_a = \frac{(m_{ab})(v_{aw})}{v_{awb}}$$

$$W_a = \frac{(0.0000)(50)}{200}$$

$$W_a = 0.0000g$$

where:

- W_a = particulate mass in acetone wash, blank corrected (g)
- m_{ab} = mass collected, acetone wash blank (g)
- v_{aw} = volume of acetone wash (ml)
- v_{awb} = volume of acetone wash blank (ml)

Mass in Front Half, Acetone Blank Corrected

$$m_f = m_{fil} + (m_a - W_a)$$

$$m_f = 0.0069 + (0.0089 - 0.0000)$$

$$m_f = 0.0159g$$

where:

- m_f = mass in front half filter, and acetone wash, blank corrected (g)
- m_{fil} = mass in front half filter (g)
- m_a = mass in acetone wash (g)
- W_a = particulate mass in acetone wash blank (g)

Total Particulate Catch

$$M_n = m_f + m_b$$

$$M_n = 0.159 + 0.0132$$

$$M_n = 0.0291g$$

where:

- M_n = total mass catch (g)
- m_f = mass in front half filter, and acetone wash, blank corrected (g)
- m_b = mass in back half organic fraction, and inorganic fraction, blank corrected (g)

Total Particulate Concentration, grains/dscf

$$C_{gr/dscf} = \frac{(M_n)(15.43)}{V_{m,std}}$$

$$C_{gr/dscf} = \frac{(0.0291)(15.43)}{60.27}$$

$$C_{gr/dscf} = 0.00746 \text{ grains / dscf}$$

where:

- $C_{gr/dscf}$ = particulate concentration (grains/dscf)
- M_n = total particulate catch (g)
- $V_{m(std)}$ = volume of gas collected at standard conditions (scf)
- 15.43 = conversion factor (grains/g)

Calculated F_d Factor, dscf/mmBtu

$$F_d = K((K_{hd} \times H) + (K_c \times C) + (K_s \times S) + (K_n \times N) - (K_o \times O_2)) / GCV_w$$

$$F_d = 10^6 ((3.64 \times 4.76) + (1.53 \times 74.64) + (0.57 \times 3.87) + (0.14 \times 1.56) - (0.46 \times 6.41)) / 12,862$$

$$F_d = 10,185$$

where:

- F_d = calculated fuel factor (dscf/mmBtu)
- K = conversion factor (Btu/million Btu)
- K_{hd} = constant (scf/lb)
- H = weight percent hydrogen in coal (%)
- K_c = constant (scf/lb)
- C = weight percent carbon in coal (%)
- K_s = constant (scf/lb)
- S = weight percent sulfur in coal (%)
- K_n = constant (scf/lb)
- N = weight percent nitrogen in coal (%)
- K_o = constant (scf/lb)
- O_2 = weight percent oxygen in coal (%)
- GCV_w = gross calorific value of fuel, wet (Btu/lb)

Total Particulate Emission Rate, lb/mmBtu ⁴

$$E_{PM} = \frac{(M_n)(F_d)(20.9)}{(V_{m(std)})(453.6)(20.9 - O_2)}$$
$$E_{PM} = \frac{(0.0291)(10,185)(20.9)}{(60.27)(453.6)(20.9 - 8.17)}$$
$$E_{PM} = 0.0178 \text{ lb / mmBtu}$$

where:

- E_{PM} = total particulate matter emission rate, (lb/mmBtu)
- M_n = total particulate catch (g)
- F_d = fuel factor (dcsf/mmBtu)
- 20.9 = oxygen content of ambient air (%)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 453.6 = conversion factor (g/lb)
- % O_2 = oxygen content of the dry gas stream (%)

Total Particulate Emission Rate, lb/hr

$$E_{lb/hr} = \frac{(M_n)(Q_{dstd})(60)}{(V_{m,std})(453.6)}$$
$$E_{lb/hr} = \frac{(0.0291)(701,128)(60)}{(60.27)(453.6)}$$
$$E_{lb/hr} = 44.9 \text{ lb / hr}$$

where:

- $E_{lb/hr}$ = particulate emission rate (lb/hr)
- M_n = total particulate catch (g)
- $V_{m(std)}$ = volume of gas collected at standard conditions (scf)
- Q_{dstd} = volumetric flow rate of the dry gas stream at standard conditions (dscfm)
- 60 = conversion factor (min/hr)
- 453.6 = conversion factor (g/lb)

⁴ All particulate emission rates are calculated in a similar manner.

Sample Calculations, Method 26A, Run 1

Concentration of Hydrogen Chloride in Flue Gas (lb/dscf)

$$C_{HCl} = \frac{(M_{HCl})}{(V_{m(std)}) (10^3) (453.59)}$$

$$C_{HCl} = \frac{(0.866)}{(99.30) (10^3) (453.59)}$$

$$C_{HCl} = 1.92 \times 10^{-8} \text{ lb / dscf}$$

where:

- C_{HCl} = concentration of hydrogen chloride in flue gas (lb/dscf)
- M_{HCl} = mass of hydrogen chloride collected in sample (mg)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 10^3 = conversion factor (mg/g)
- 453.59 = conversion factor (g/lb)

Concentration of Hydrogen Chloride in Flue Gas (ppmdv)

$$C_{ppmv} = \frac{(M_{HCl})(385.3)(10^6)}{(MW_{HCl})(V_{m(std)}) (10^3) (453.59)}$$

$$C_{ppmv} = \frac{(0.866)(385.3)(10^6)}{(36.458)(99.30)(10^3)(453.59)}$$

$$C_{ppmv} = 0.203 \text{ ppmdv}$$

where:

- C_{ppmv} = concentration of hydrogen chloride in flue gas (ppmv)
- M_{HCl} = mass of hydrogen chloride collected in sample (mg)
- 385.3 = volume occupied by one pound gas at standard conditions (dscf/lbmole)
- 10^6 = conversion factor (fraction to ppm)
- MW_{HCl} = molecular weight of hydrogen chloride (lb/lb-mole)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 10^3 = conversion factor (mg/g)
- 453.59 = conversion factor (g/lb)

Hydrogen Chloride Emission Rate, lb/mmBtu

$$E_{HCl} = \frac{(C_{HCl})(F_d)(20.9)}{(20.9 - O_2)}$$

$$E_{HCl} = \frac{(1.92 \times 10^{-8})(10,185)(20.9)}{(20.9 - 8.17)}$$

$$E_{HCl} = 0.000339 \text{ lb / mmBtu}$$

where:

E_{HCl} = hydrogen chloride emission rate, (lb/mmBtu)

C_{HCl} = hydrogen chloride concentration, (lb/dscf)

F_d = fuel factor (dcsf/mmBtu)

20.9 = oxygen content of ambient air (%)

% O_2 = oxygen content of the dry gas stream (%)

Hydrogen Chloride Emission Rate

$$E_{HCl} = C_{HCl} \times Q_{dstd} \times 60$$

$$E_{HCl} = 1.92 \times 10^{-8} \times 700,731 \times 60$$

$$E_{HCl} = 0.808 \text{ lb / hr}$$

where:

E_{HCl} = hydrogen chloride emission rate, (lb/hr)

C_{ppmvd} = hydrogen chloride concentration, dry basis, (ppmvd)

Q_{dstd} = volumetric flow rate of the dry gas stream at standard conditions (dscfm)

MW = molecular weight of hydrogen chloride (lb/lbmole)

60 = conversion factor (min/hr)

385.3 = volume occupied by one pound gas at standard conditions (dscf/lbmole)

10^6 = conversion factor (fraction to ppm)

Sample Calculations, Method 29, Run 1

Concentration of Lead in Flue Gas, ug/dscm⁵

$$C_{ug/dscm} = \frac{(M_c)}{(V_{m(std)})} (35.31)$$

$$C_{ug/dscm} = \frac{(5.00)}{(69.26)} (35.31)$$

$$C_{ug/dscm} = 2.55 \text{ ug / dscm}$$

where:

- $C_{ug/dscm}$ = concentration of lead in flue gas (ug/dscm)
- M_c = mass of lead in sample (ug)
- $V_{m(std)}$ = volume of gas collected at standard temperature and pressure (scf)
- 35.31 = conversion factor (ft³/m³)

Emission Rate of Lead in Flue Gas, lb/mmBtu⁶

$$E = \frac{(C_{ug/dscm})(F_d)(20.9)}{(35.315)(20.9 - \%O_2)(453.6)(10^6)}$$

$$E = \frac{(2.55)(10,185)(20.9)}{(35.315)(20.9 - 8.17)(453.6)(10^6)}$$

$$E = 2.66 \times 10^{-6} \text{ lb / mmBtu}$$

where:

- E = lead emission rate (lb/mmBtu)
- $C_{ug/dscm}$ = lead concentration (ug/dscm)
- F_d = fuel factor (dscf/mmBtu)
- 35.315 = conversion factor (ft³/m³)
- 20.9 = oxygen content of ambient air (%)
- %O₂ = oxygen content of the dry gas stream (%)
- 453.6 = conversion factor (g/lb)
- 10⁶ = conversion factor (ug/g)

⁵ The concentrations of all MHs and mercury are calculated in a similar manner.

⁶ The emission rates of all MHs and mercury are calculated in a similar manner.

Lead Emission Rate, lb/hr

$$E_{lb/hr} = \frac{(C_{ug/dscm})(Q_{dstd})(60)}{(35.31)(10^6)(453.6)}$$

$$E_{lb/hr} = \frac{(2.55)(722,850)(60)}{(35.31)(10^3)(10^3)(453.6)}$$

$$E_{lb/hr} = 0.00690 lb/hr$$

where:

- $E_{lb/hr}$ = lead emission rate (lb/hr)
- $C_{ug/dscm}$ = lead concentration (ug/dscm)
- Q_{dstd} = volumetric flow rate of dry gas stream at standard conditions (dscfm)
- 10^3 = conversion factor (ug/mg)
- 10^3 = conversion factor (mg/g)
- 35.31 = conversion factor (ft³/m³)
- 60.0 = conversion factor (min/hr)
- 453.59 = conversion factor (g/lb)